

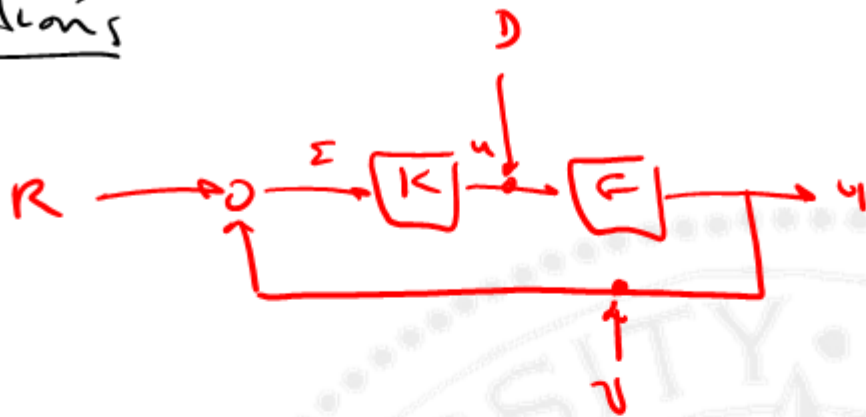
CMPE-242

Applied Feedback Control

Gabriel Hugh Elkaim

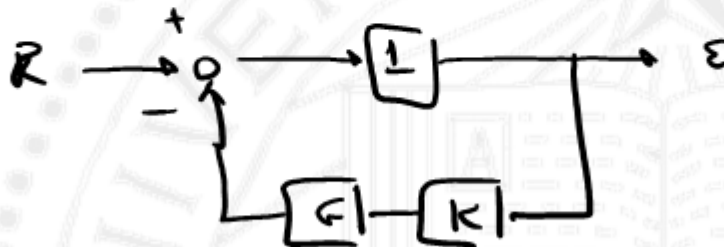


Questions



$$\frac{Y}{R} = \frac{GK}{1+GK}$$

2/1/5



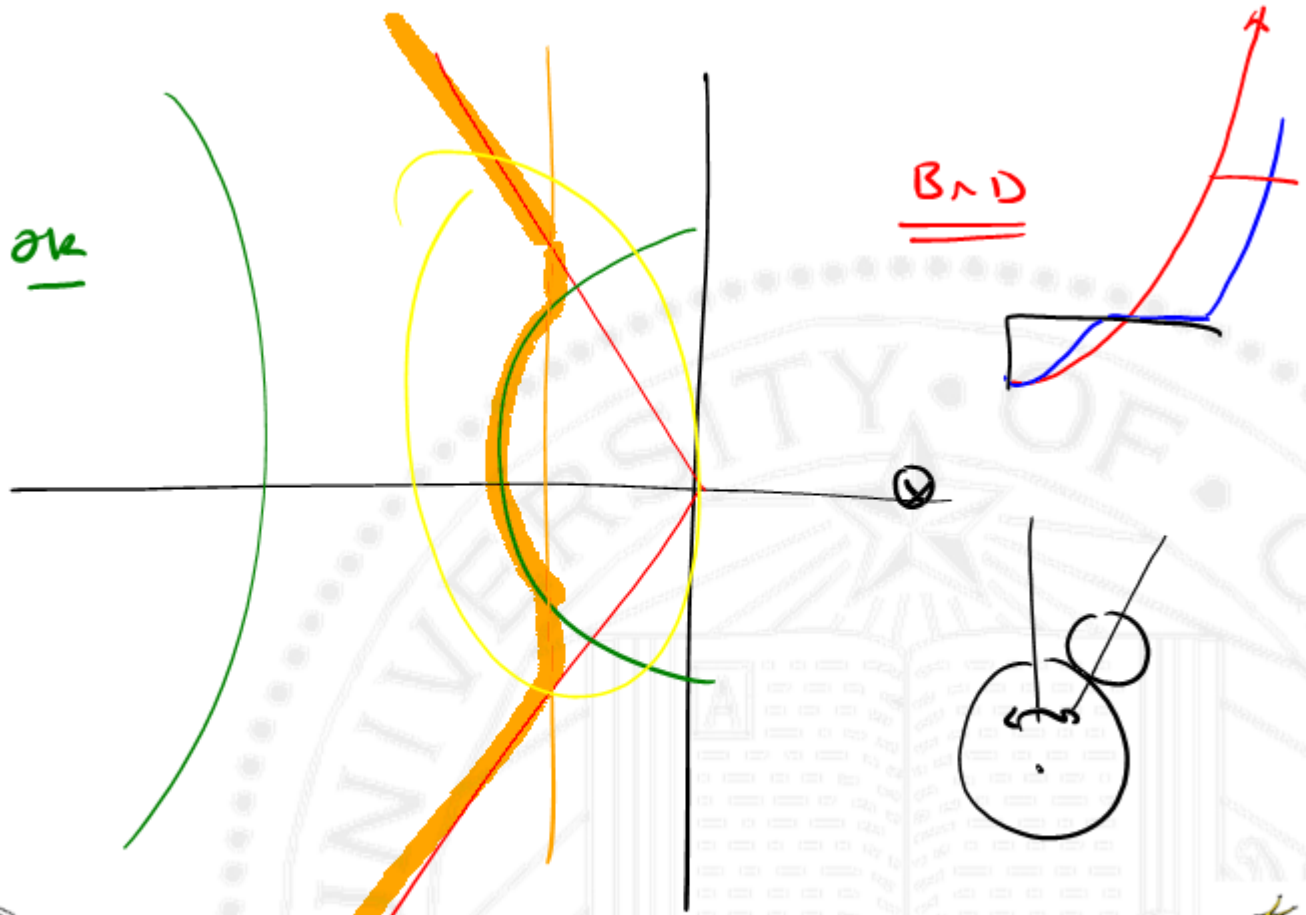
$$\frac{\Sigma}{R} = \frac{1}{1+GK}$$

$$\Sigma_{SS} = \text{FVT} \rightarrow \lim_{s \rightarrow 0} s \left[\frac{\Sigma}{R} \right] R(s) \quad \uparrow \quad Y_s$$



ok

B > D

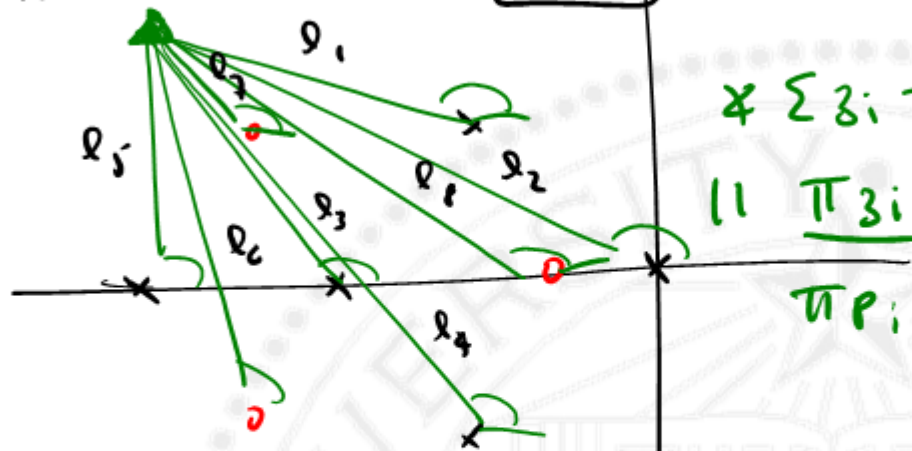


ROOT LOCUS

$$\Delta_d(s) = 1 + GK = 0 \therefore \boxed{GK = -1}$$

$$\angle \pm 180$$

$$1 \cdot 1 = 1$$



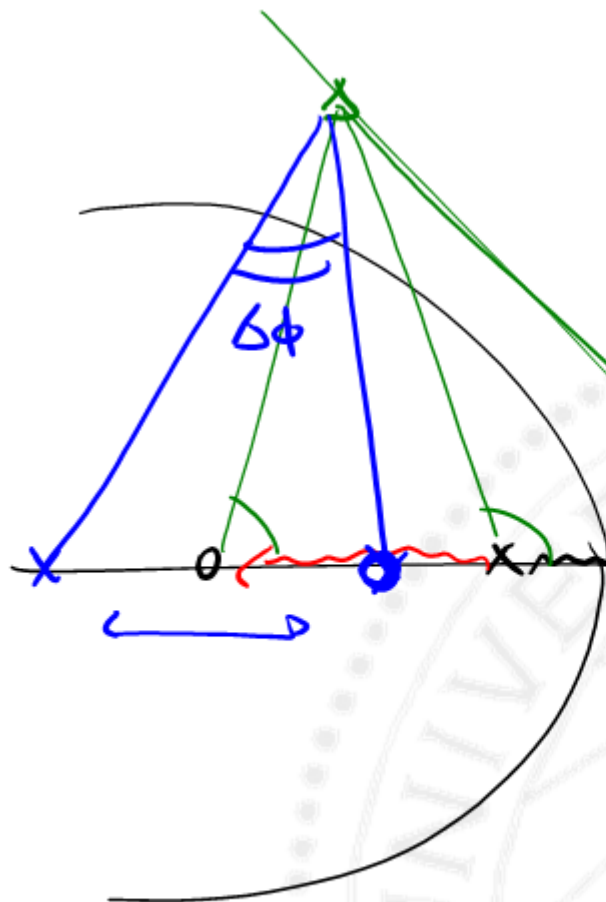
$$\angle \sum z_i - \sum p_i$$

$$\parallel \frac{\pi z_i}{\pi p_i}$$

$$\pi p_i$$

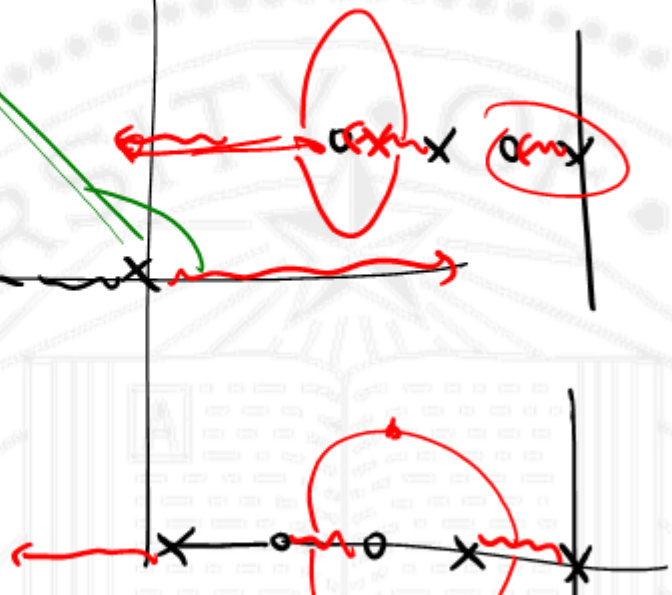
$$GK \Big|_s = \frac{z_0 z_1 z_2}{p_1 p_2 p_3 p_4 p_5} e^{-j(\phi_0 + \phi_1 + \phi_2 - \phi_3 - \phi_4 - \dots - \phi_5)}$$

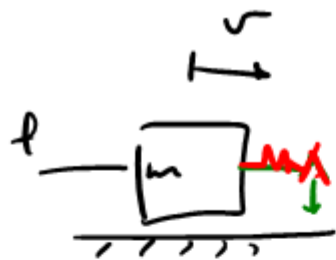




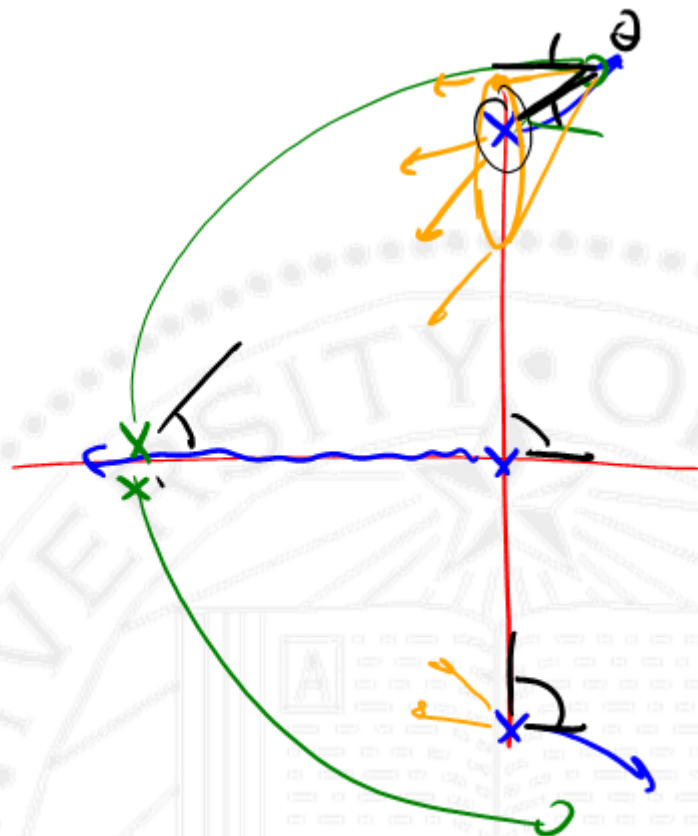
XDD ~ WxD

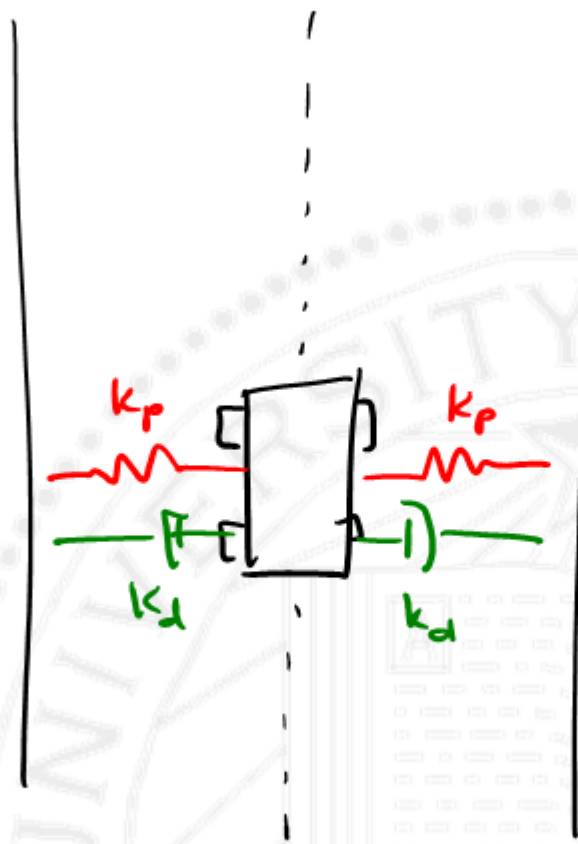
indicated angle $\Delta\phi$





$$\phi_d \sim f(\theta)$$





k_p "spring"

k_b "dampers"

k_i - kill steady state error.



BODE — TRACKING SPEC'S / ROBUSTNESS
 — MODEL FREE DESIGN

ROOT LOCUS



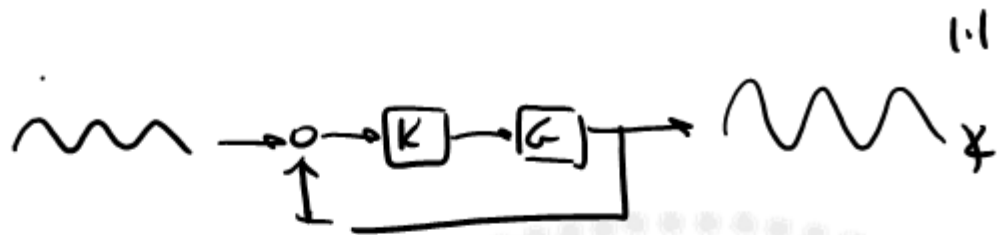
$$1 + GK = 0 \rightarrow GK = -1$$

2 1p0
|| 2

$$KG = \frac{K(n+a)(n+b)}{(s+c)(s+d)(s+e)} = K \frac{k_a k_b}{k_c k_d k_e} e^{j(\phi_a + \phi_b - \phi_c - \phi_d - \phi_e)}$$



Bode:



$$\frac{Y}{R} = \frac{GK}{1+GK}$$

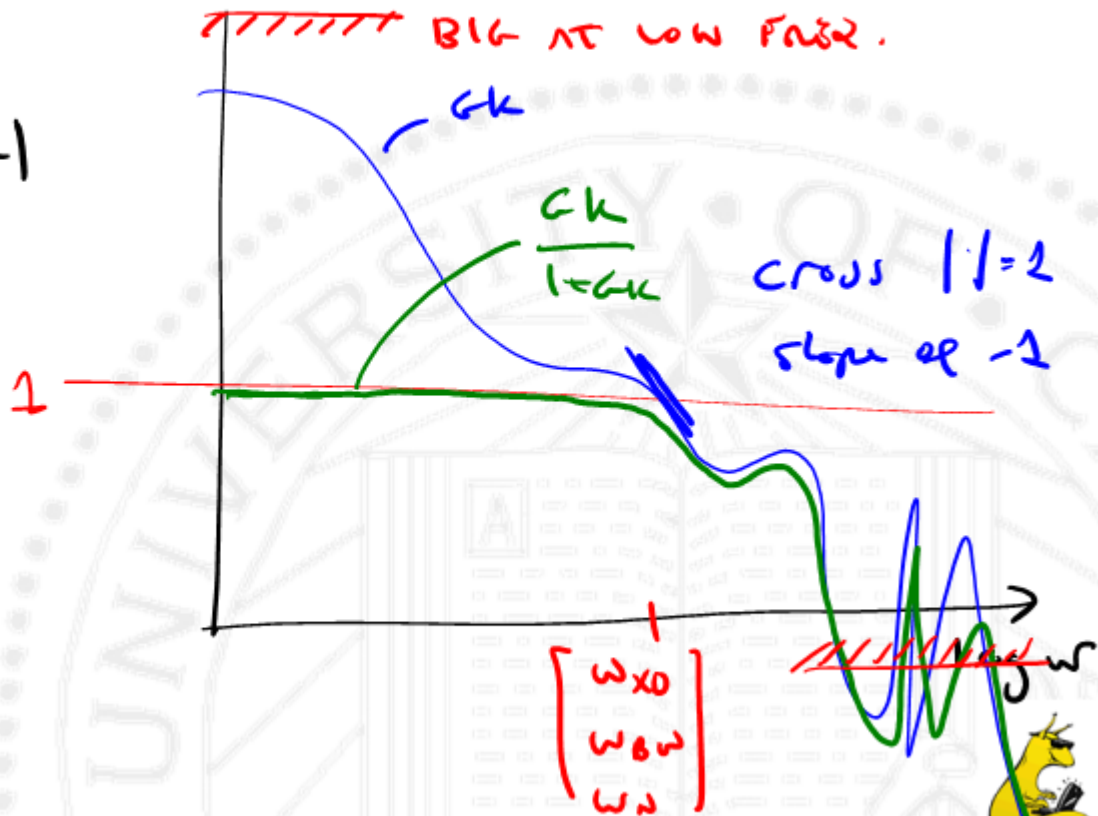
if $|GK|$ big

$$\frac{GK}{1+GK} \approx 1$$



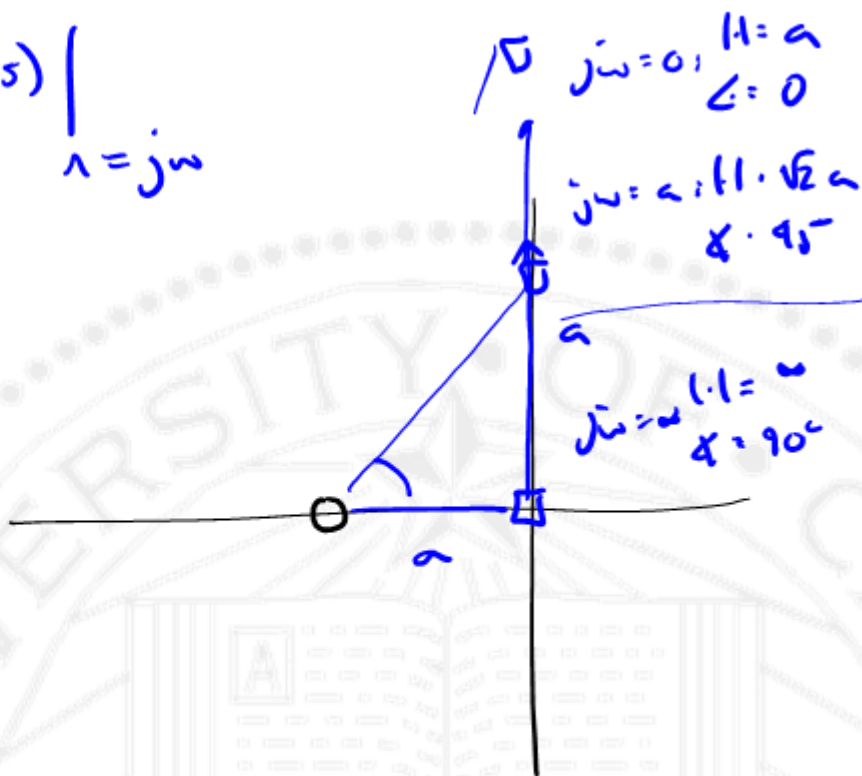
BODE DESIGN

$\log |GK|$



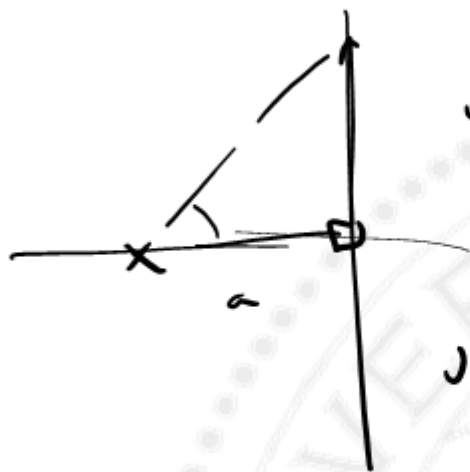
$$Bode \rightarrow G(s) \quad | \quad s = j\omega$$

$$G(s) = s + a$$



$$G(s) = \frac{1}{s+a}$$

$$j\omega = 0 \rightarrow |L| = \frac{1}{a}$$
$$\angle = 0$$



$$j\omega = a \quad |L| = \frac{1}{\sqrt{2}a}$$

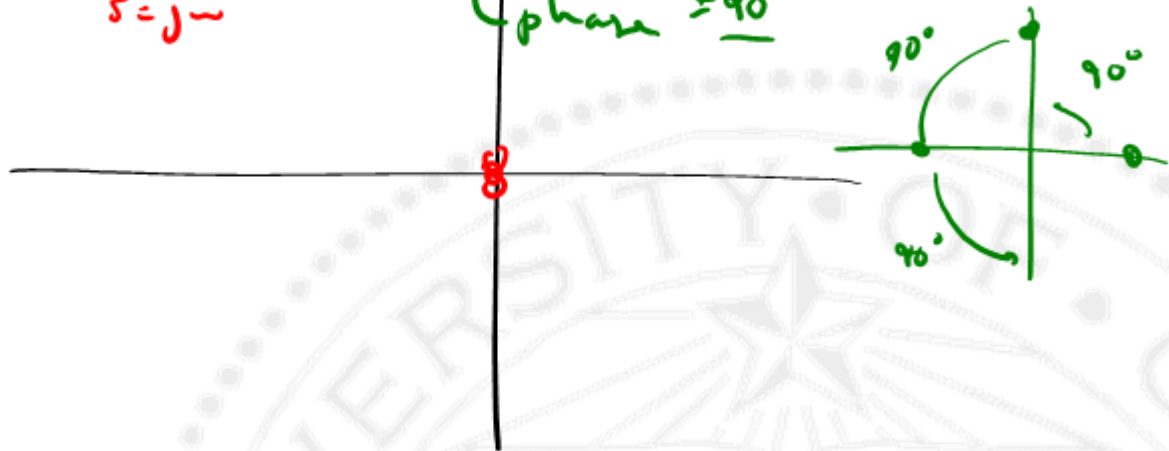
$$\angle = -90^\circ$$

$$j\omega = \infty \quad |L| = 0$$

$$\angle = -90^\circ$$



$$s^n \Big|_{s=j\omega} = (j\omega)^n = \underbrace{(j^n)}_{\text{phase } \pm 90^\circ} \underbrace{(\omega^n)}_{\text{magnitude}}$$



$$\log(\omega^n) = n \frac{\log \omega}{1}$$

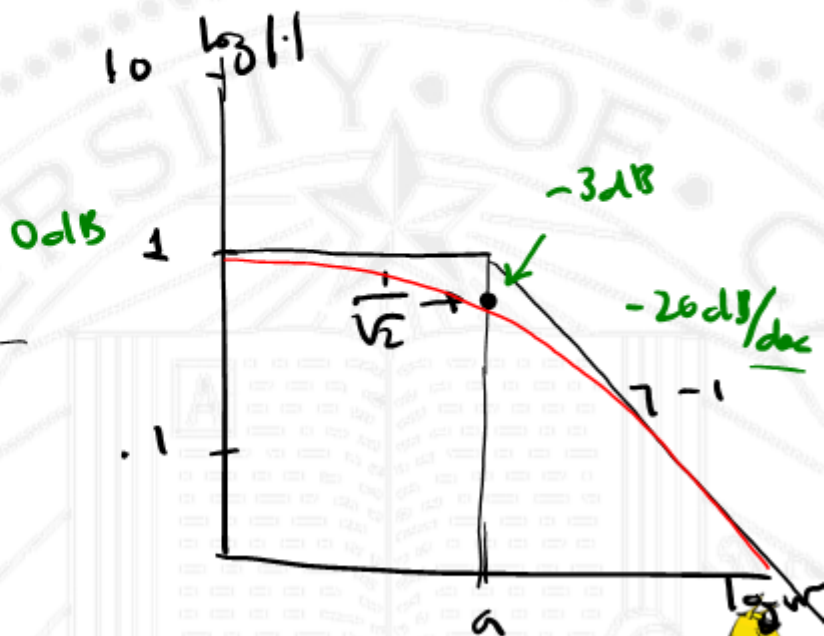
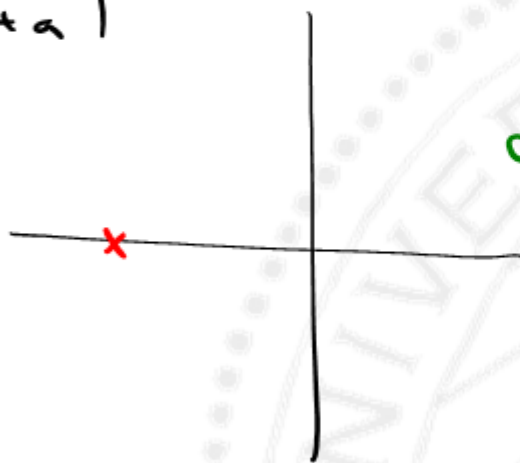
↑
straight lines



$\| - \log \|$ vs $\log \omega$

$\angle - \phi$ vs $\log \omega$

$$\left(\frac{a}{s+a} \right)$$

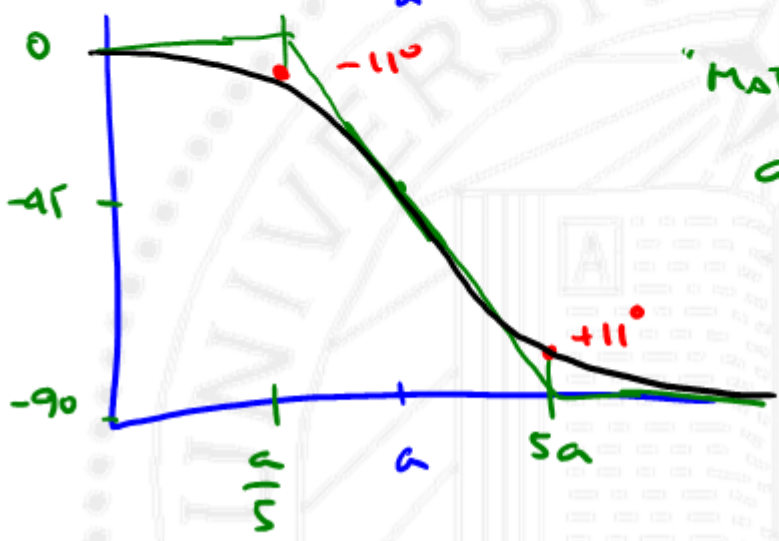


$\log ||$



"single pole"
magnitude

ϕ

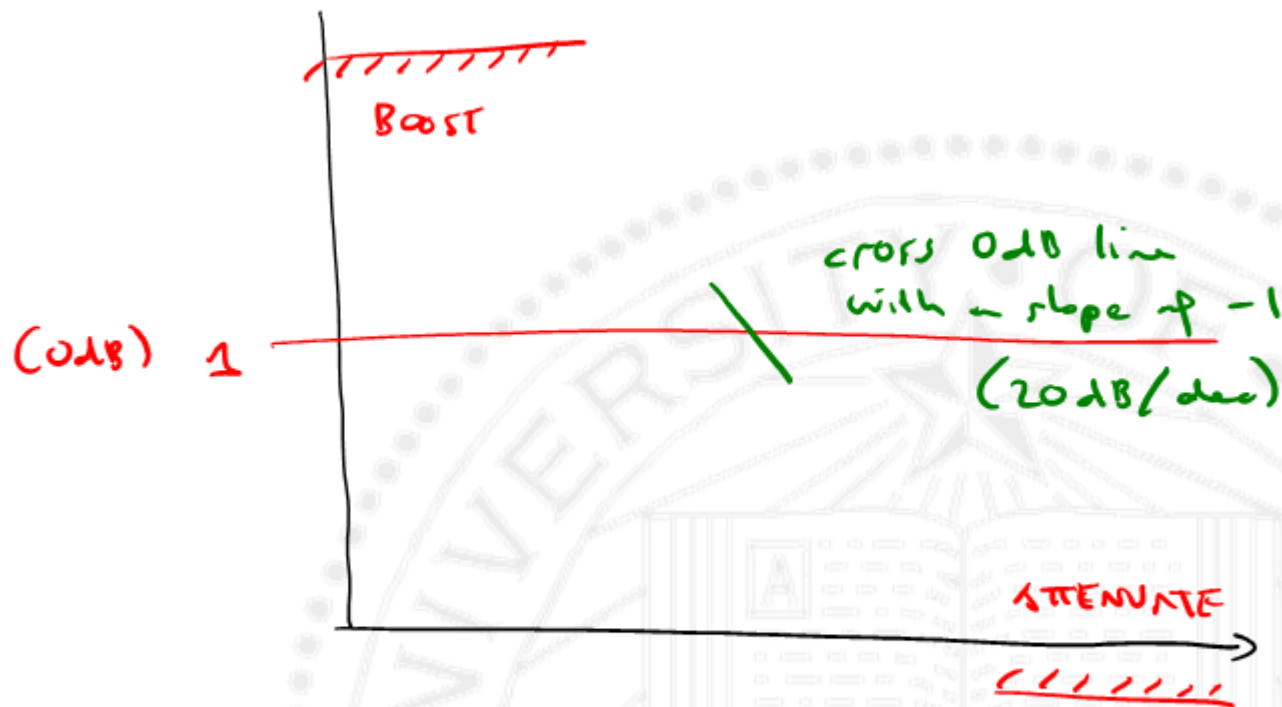


"MATCHED INFLECTION"
 $a e^{-\pi/2}$ $a e^{\pi/2}$

phase



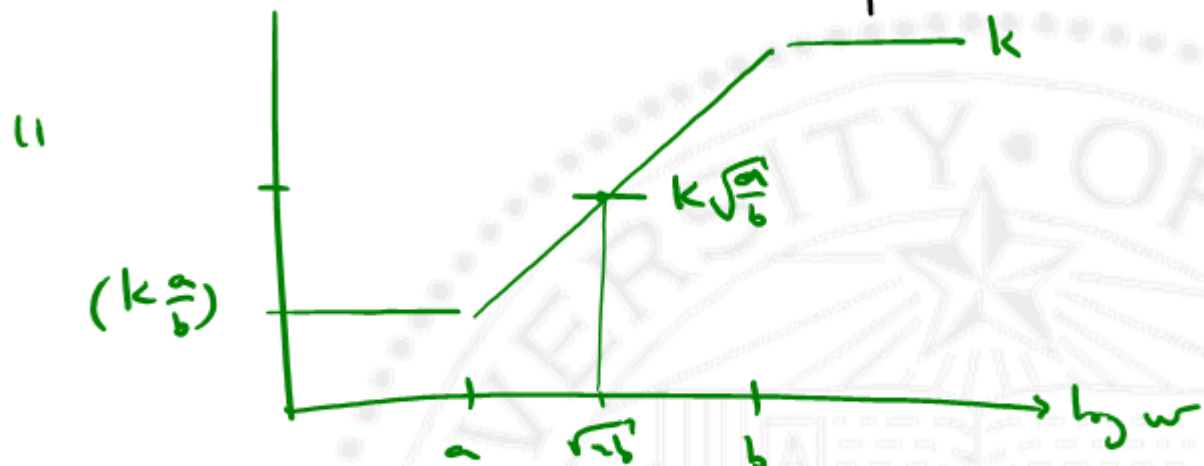
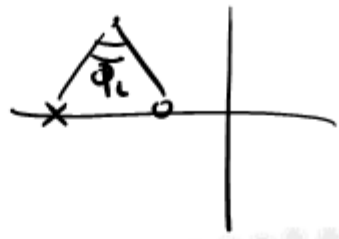
BODE DESIGN



LEXD

$$K \frac{s+a}{s+b}$$

$b > a$

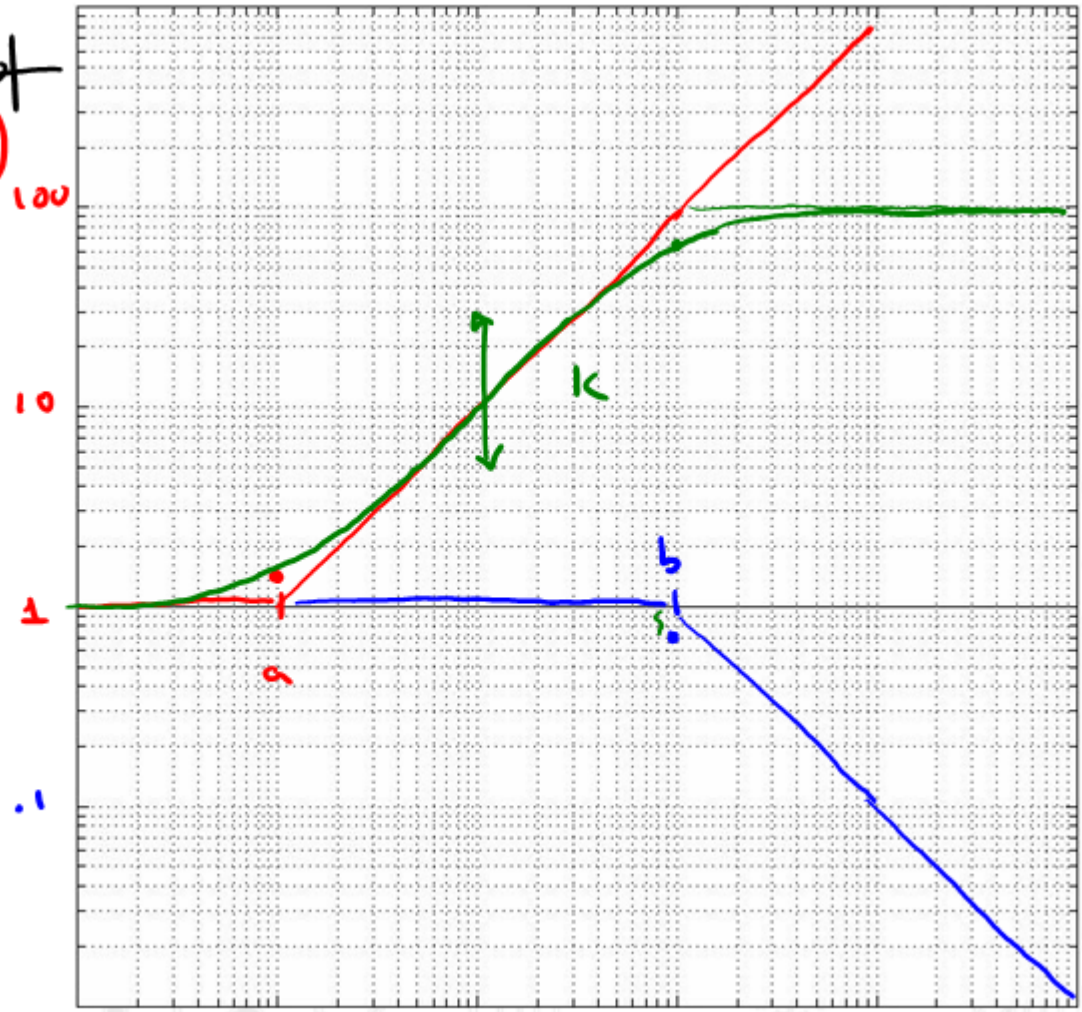


LEAD: $\times 10^{\frac{b}{a}}$

$$k \frac{s+a}{s+b} \left(\frac{b}{a}\right)$$

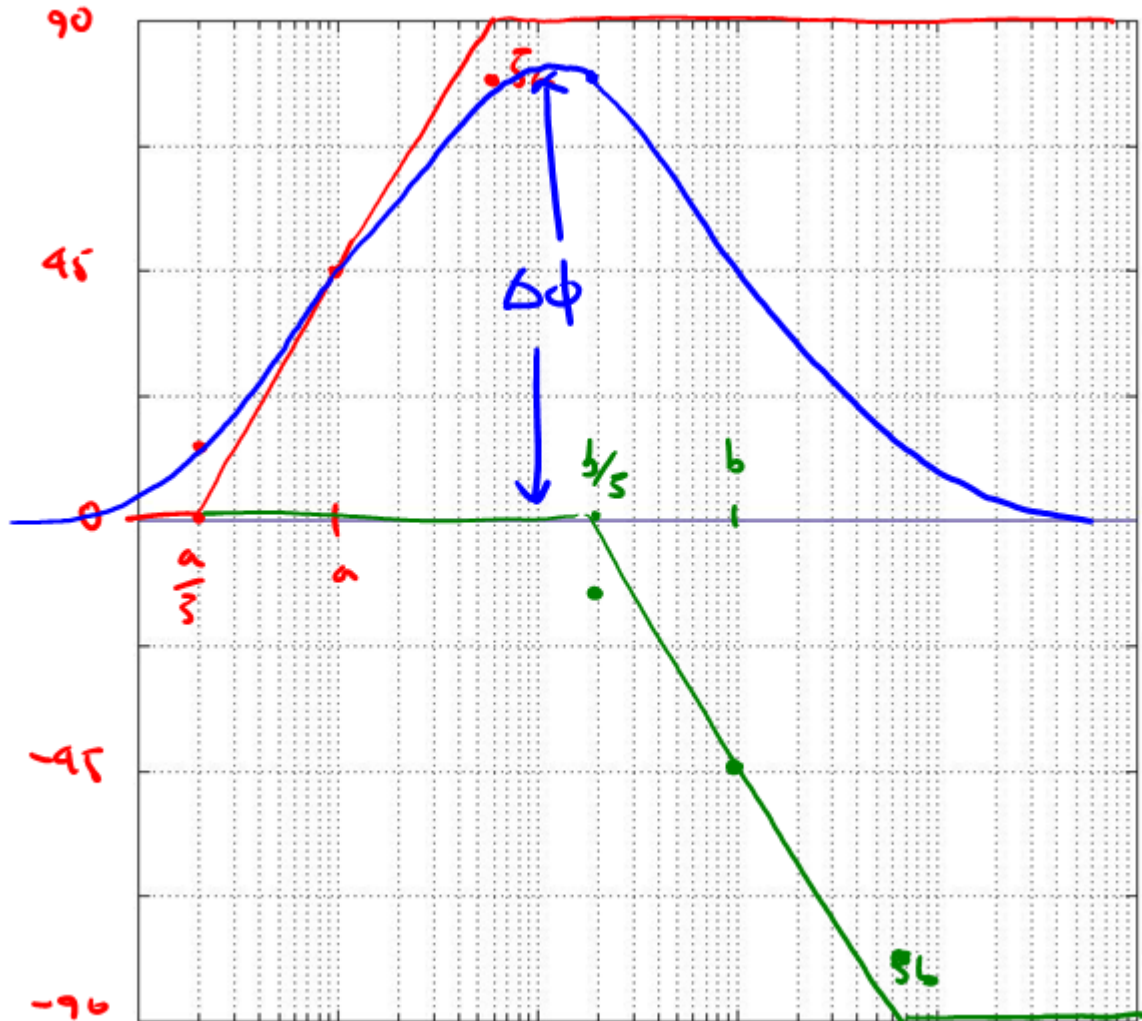
$$\left(\frac{s+a}{a}\right)$$

$$\frac{b}{s+a}$$



0 dB





$$\underline{LEAD} \quad K \frac{s+a}{s+b}$$

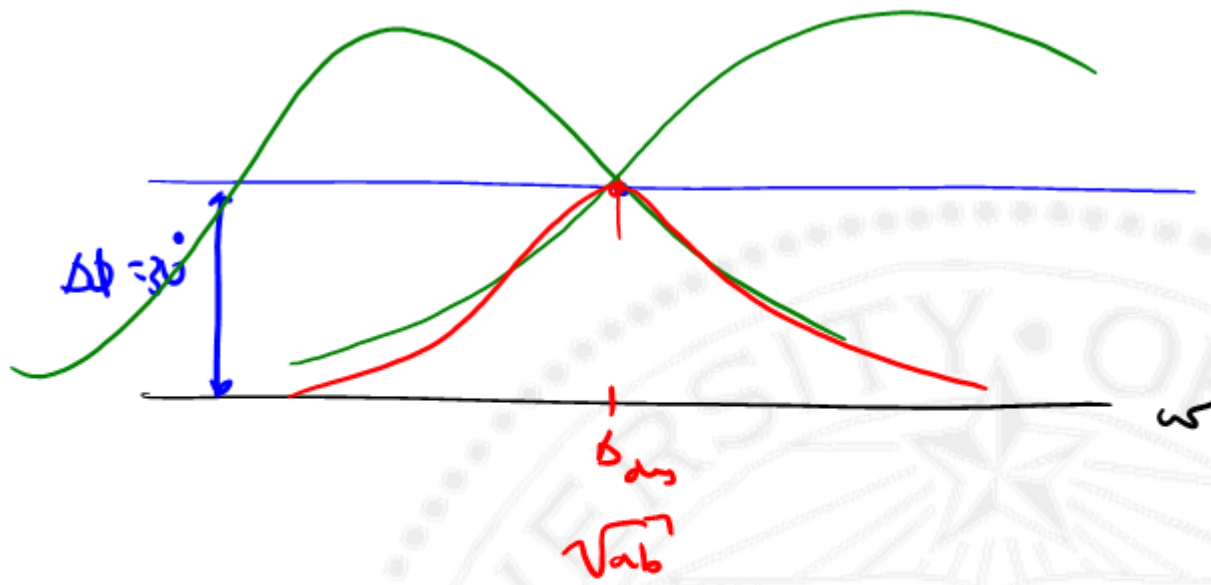
$$\text{choose } K = \sqrt{\frac{b}{a}} \quad \frac{2}{\sqrt{s}}$$

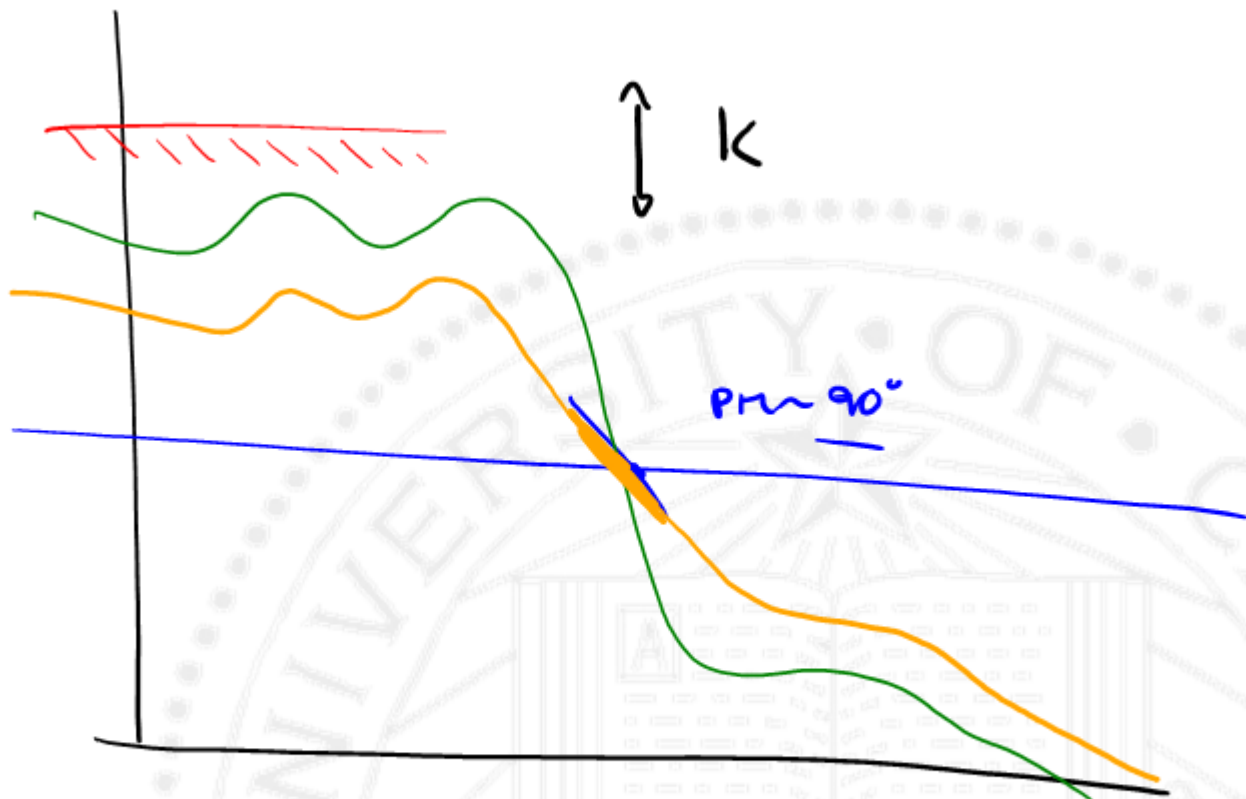
UNITY GAIN

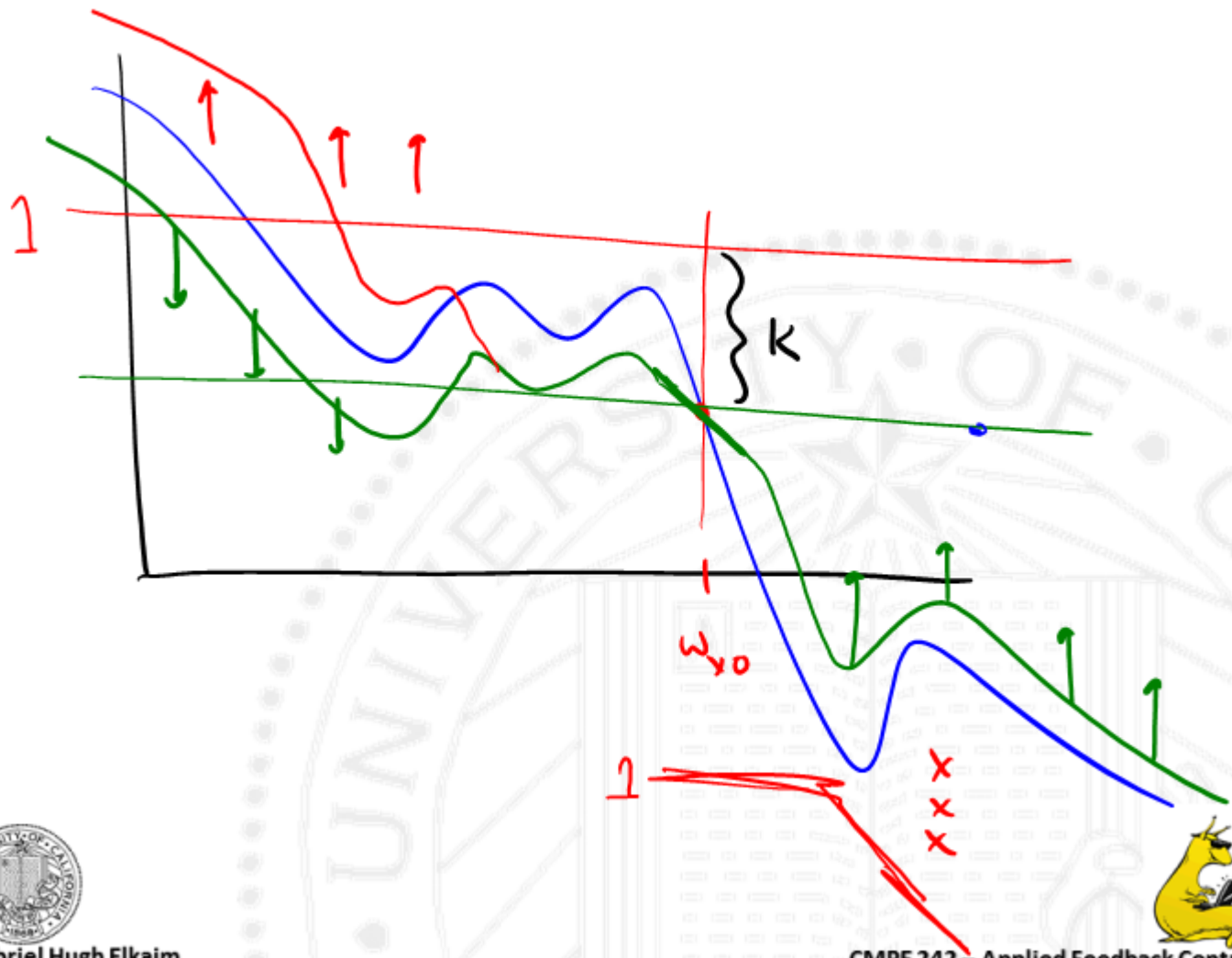
@ \sqrt{ab}

(b/a)	ΔPM
4	36°
10	55°
25	68°
50	72°





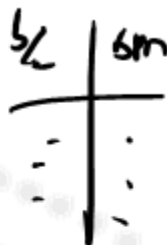




BODE DESIGN

(1) GAIN FOR ω_{x0} (K)

(2) LEAD FOR PM $\rightarrow K_{LEAD} = \sqrt{\frac{b}{a}}$ $\omega_{x0} = \sqrt{ab}$



(3) LAG FOR LOW FREQ. GAIN

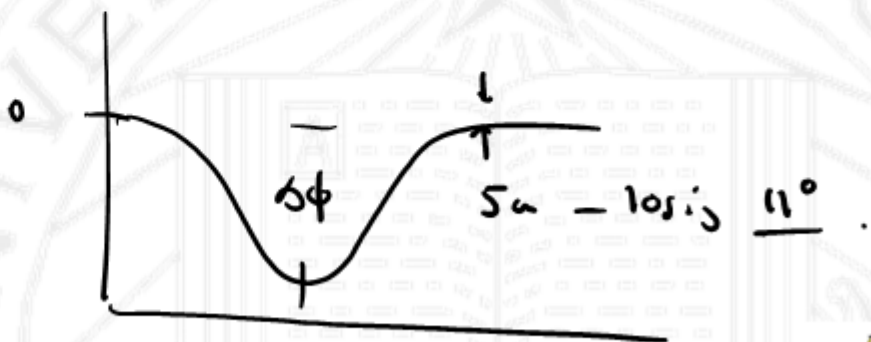
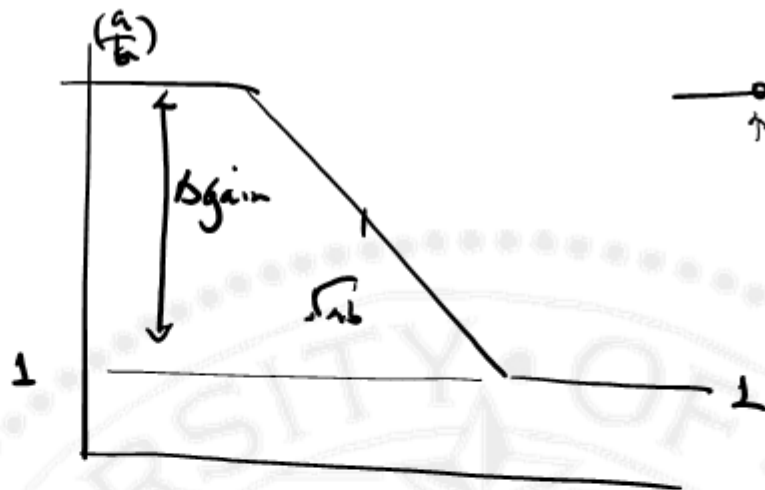
@ $5a \rightarrow$ lose 11° of phase

(4) LAG OR POLES @ HIGH FREQUENCIES



LAG

$$\left(\frac{s+a}{s+b} \right)$$

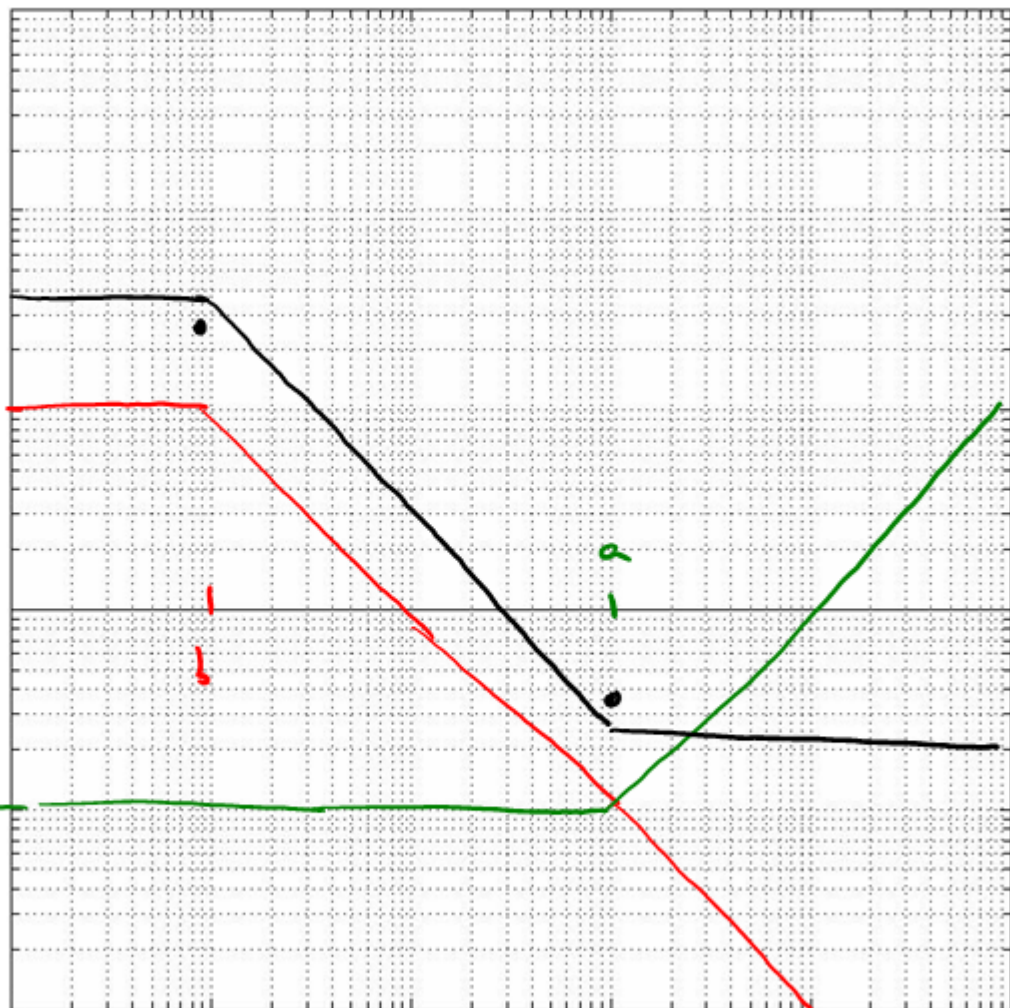


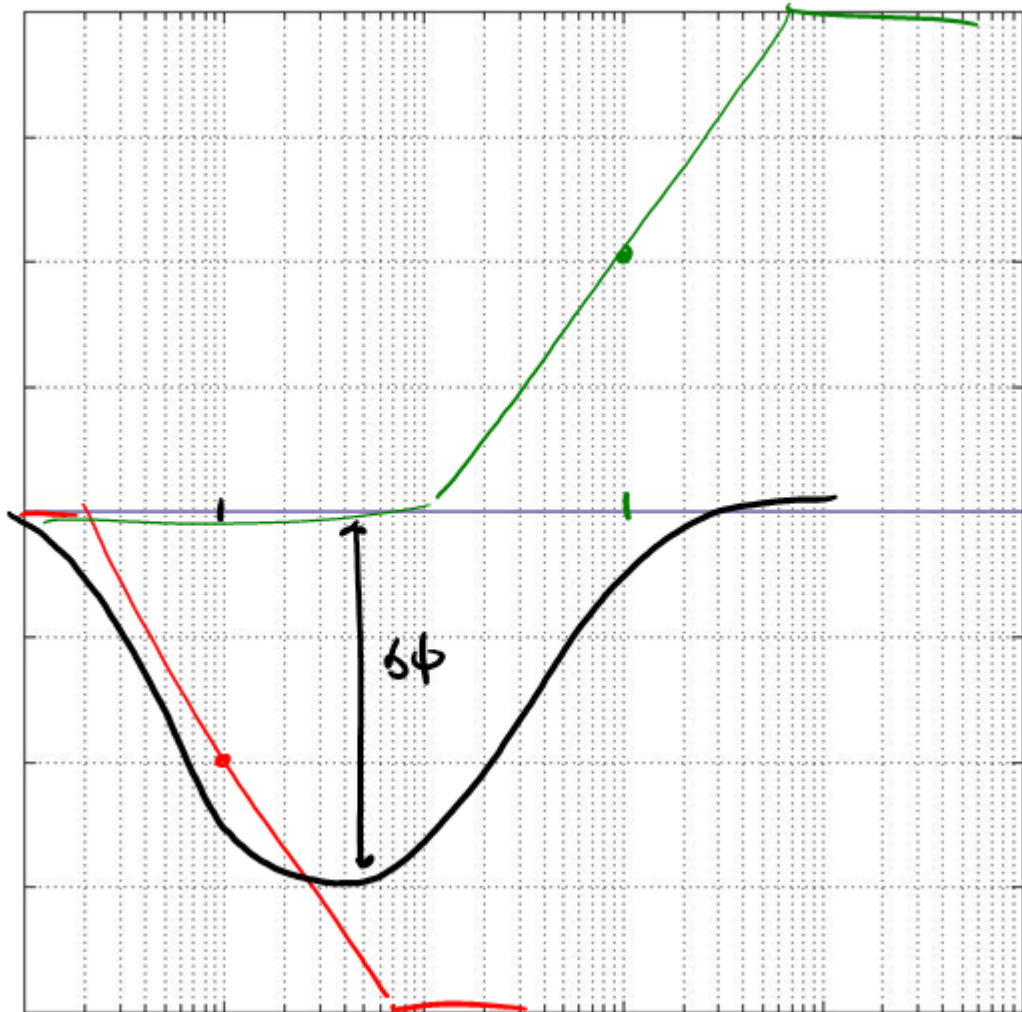
$$\frac{LAG}{s+a}$$

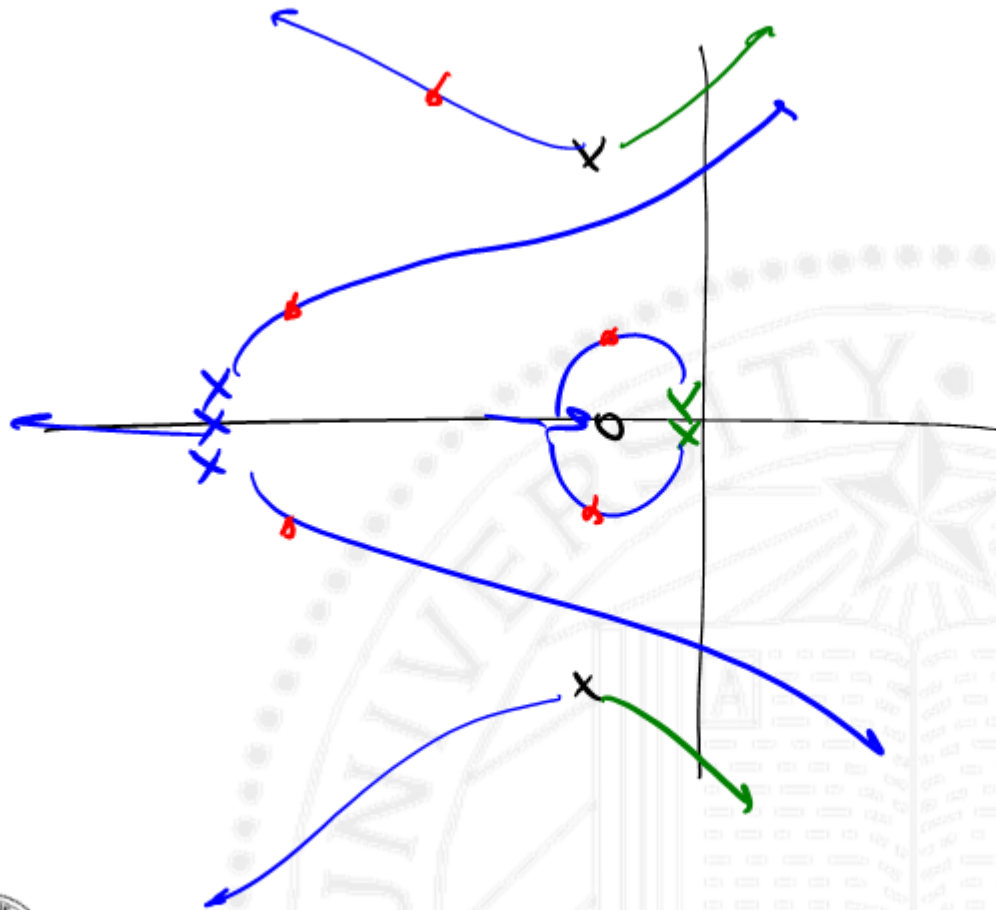
$(\frac{1}{s})$

$-1/s$

g

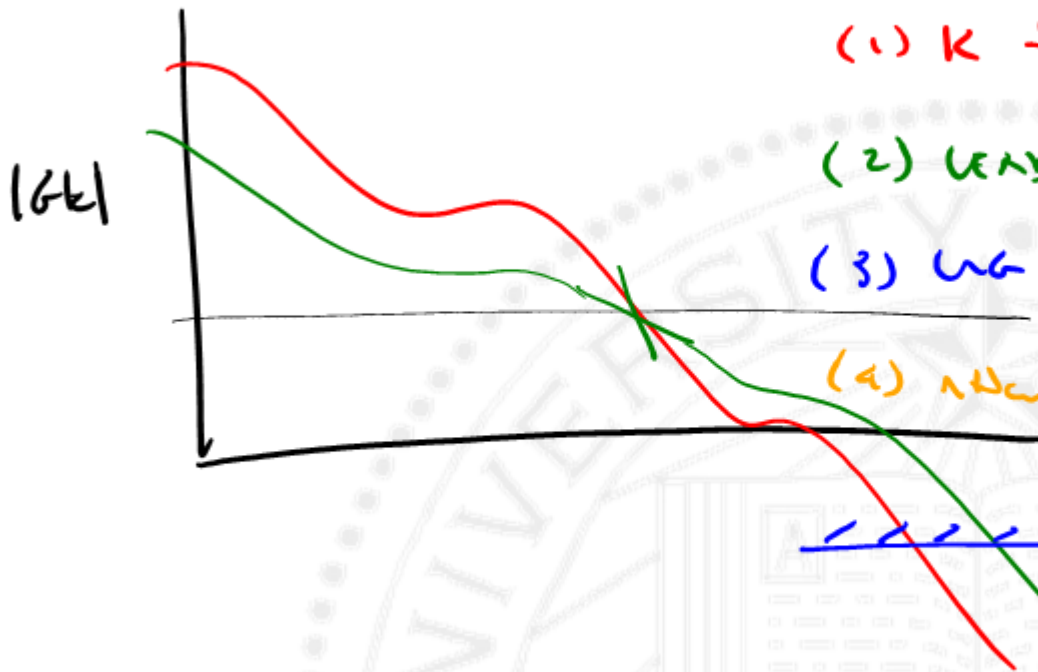






OPEN LOOP BODE

$|GK|$



(1) K to hit ω_{x0}
BW

(2) LEAD to hit ω_{PM}

(3) ω_{GB} to hit low

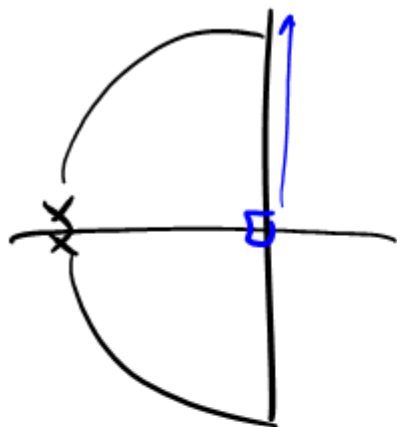
freq. gain

(4) Attenuate

high freq.

high or power





$$\frac{\omega_n^2}{s^2 + 2j\omega_n s + \omega_n^2}$$

$$j\omega = 0: \quad |1| = 1$$

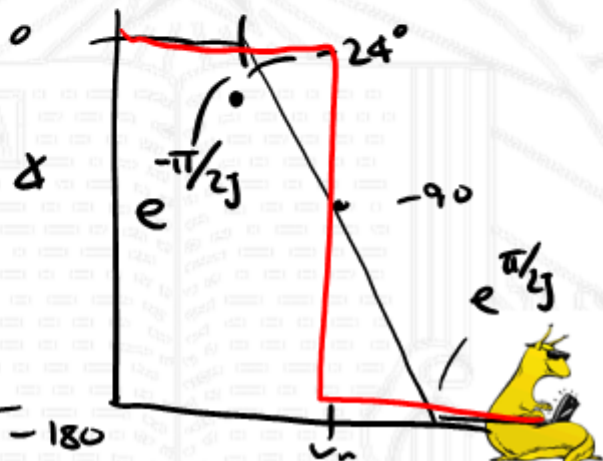
$$\quad \quad \quad \angle = 0^\circ$$

$$j\omega = \omega_n: \quad |1| = \frac{1}{2j} \quad (Q)$$

$$\quad \quad \quad \angle = -90^\circ$$

$$j\omega = \infty: \quad |1| = 0$$

$$\quad \quad \quad \angle = 180^\circ$$



$$G(s) = \frac{(s+1) \cdot 5^2}{s^2 + 2(.25)s + 5^2}$$

