

CMPE-242

Applied Feedback Control

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Announcements

- Three handouts —
- (1) Course Course Info
 - (2) Detailed Syllabus
 - (3) Prerequisite

Differential Equations (CCODE)

Pre req's — Laplace Transforms

Complex Numbers

Linear Algebra — Det/Eig/Inver

Fourier Analysis

$$a + bj$$
$$Ae^{i\theta}$$



Announcements (cont.)

Grading: — A/B/F

MATLAB — Control System Toolbox

SISO TOOL

Structural class time



Intro

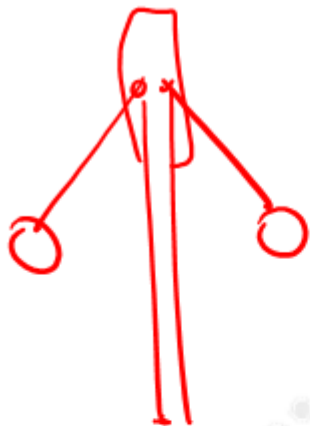
Classical Control { Transfer functions
Root locus
Bode
Nyquist 3 weeks

Digital Control { z-transform
equivalence 3 weeks

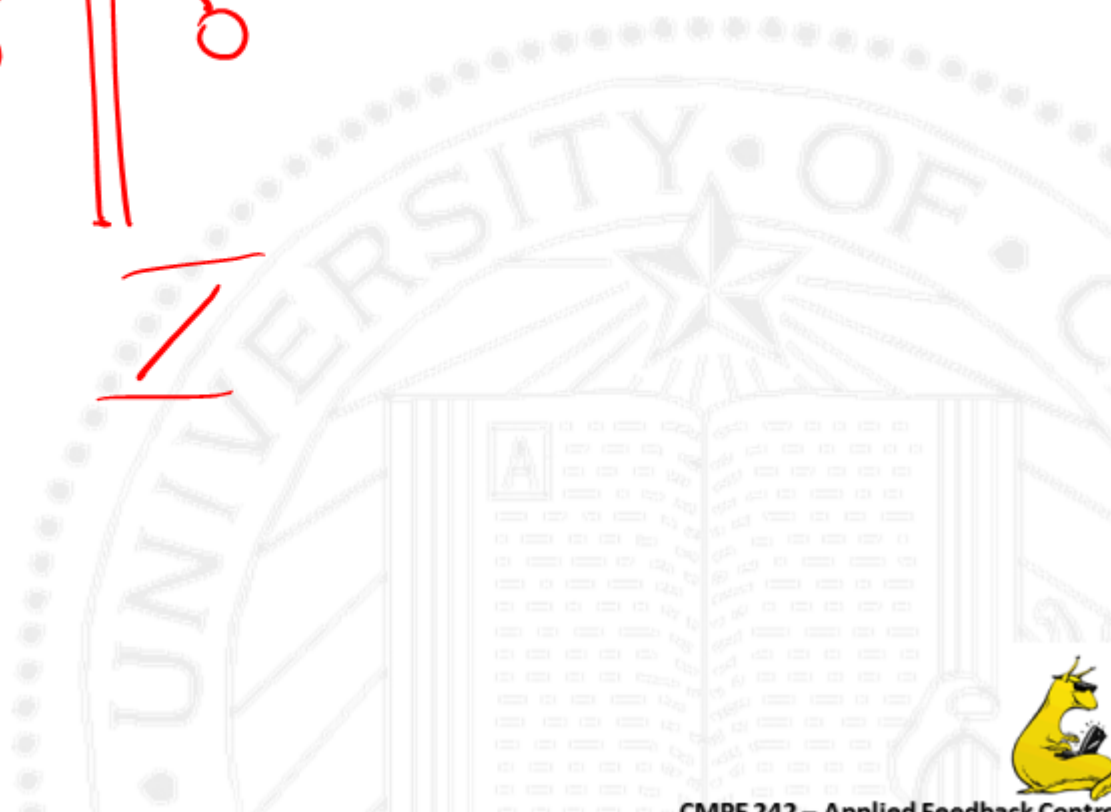
State Space { "Modern STC" - 1960's
Linear Algebra
 $\mathcal{L}(\cdot) \rightarrow R/E/G$

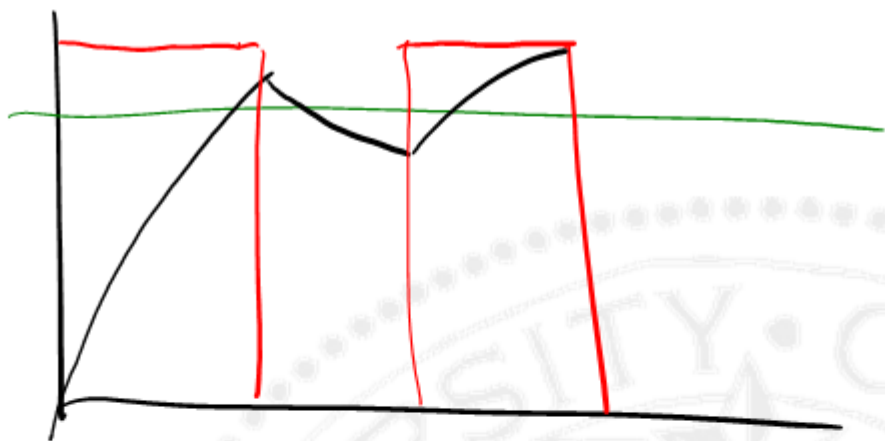
Not covered: Non-linear control (Lyapunov)
Bang/Bang +/0/-





Flyball Governor



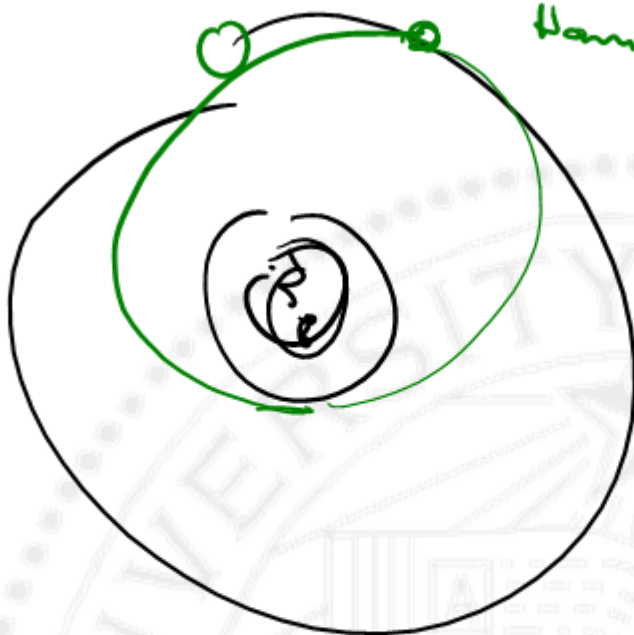


Art Bryson - calculus of variations

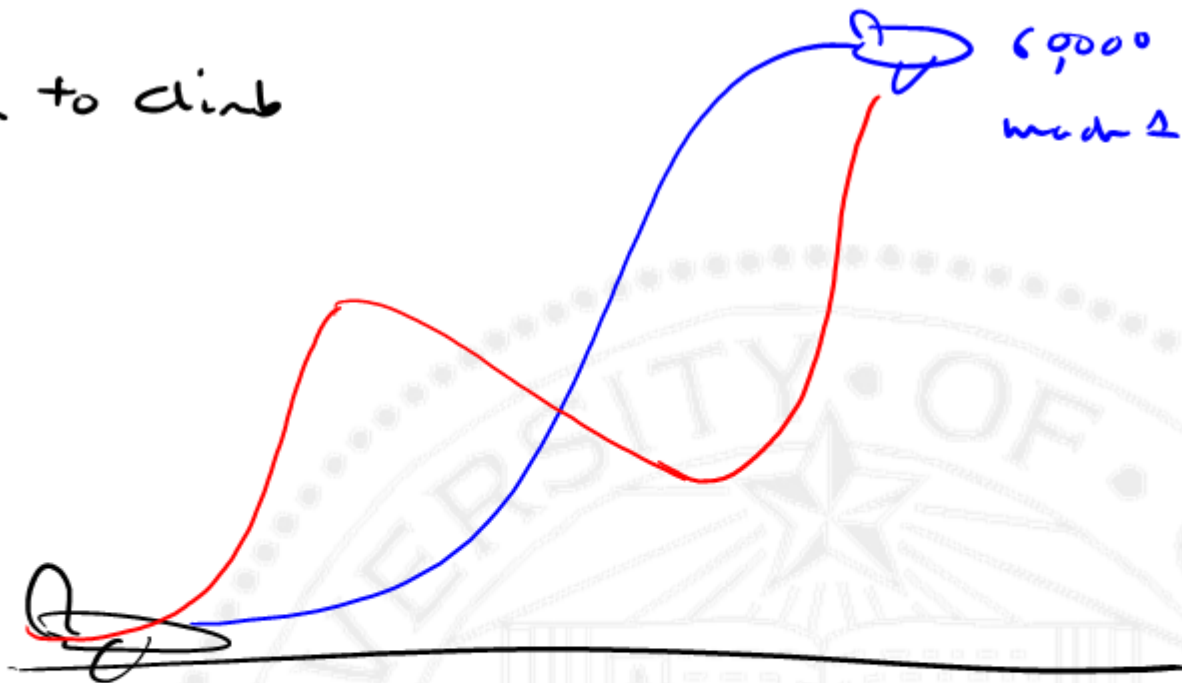
$$\int_0^{\infty} J + \lambda_i \text{ constraints}$$



Hankman Transfer



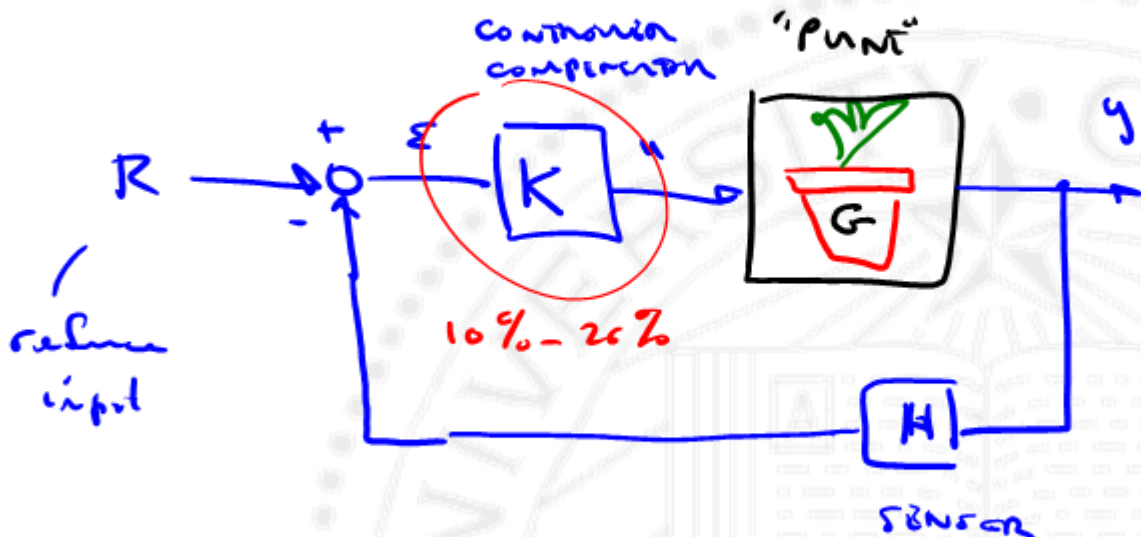
Time to climb



6000
meters



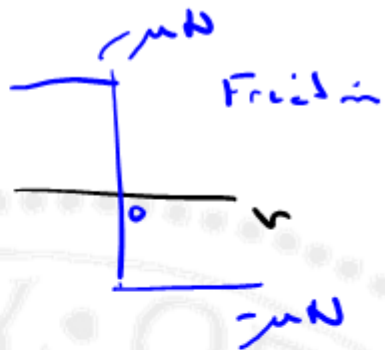
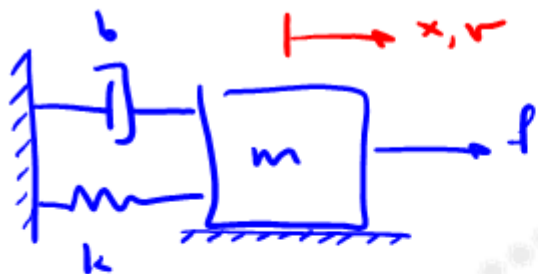
CONTROLS \neq APPLIED MATH



READ FPE ch. 1-3



Equations of Motion



$$F = \frac{d\vec{p}}{dt} = m \ddot{x}$$

$$F_f = \mu N \operatorname{sign}(v)$$

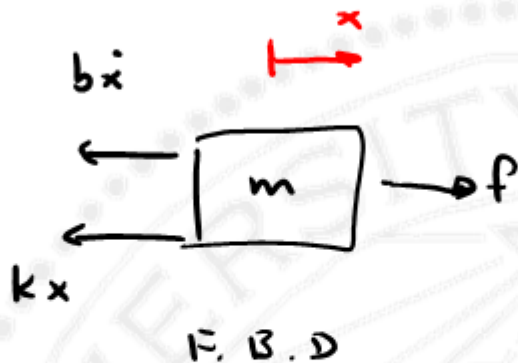
$$F = b \dot{x}$$

$$F = -kx$$

$$= k \int v dt$$



$$\Sigma F = m \ddot{x} = f - b \dot{x} - kx$$



$$\underbrace{m \ddot{x} + b \dot{x} + kx}_{\substack{\uparrow \quad \uparrow}} = f$$





↑
 v_{out}
 ↓

Kirchoff's Laws

$$\sum i_{\odot} = \phi$$

$$\sum v_{\odot} = \phi$$

⊥ $i = C \dot{v}$

~ $i = v/R$

∞ $i = \frac{1}{L} \int v dt$



Equations of Motion

$$F = m\ddot{x} + b\dot{x} + kx$$

Linear, constant coefficient ordinary Diff. Eq'n.
(CCODE)

"LINEAR TIME INVARIANT" - LTI

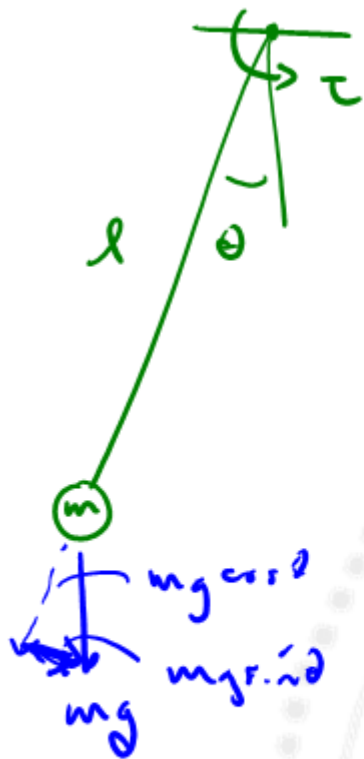
$$F_1 \longrightarrow x_1$$

$$F_2 \longrightarrow x_2$$

$$F_1 + F_2 \longrightarrow x_1 + x_2$$

$$\alpha F_1 \longrightarrow \alpha x_1$$





$$m l^2 \ddot{\theta} + m g l \sin \theta = \tau$$

$$\theta \triangleq \theta_0 + \delta \theta$$

\uparrow constant \uparrow small

$$\tau \triangleq \tau_0 + \delta \tau$$

$$\sin(\theta_0 + \delta \theta) = \sin \theta_0 \cos \delta \theta + \cos \theta_0 \delta \theta$$

$$m g l \sin \theta_0 = \tau_0$$

$$\theta_0 = \sin^{-1} \left(\frac{\tau_0}{m g l} \right)$$



$$m l^2 \ddot{\theta} + m g l (\sin \theta_0 + \cos \theta_0 \delta \theta) = \tau_0 + \delta \tau$$

$$m l^2 \ddot{\theta} + \cancel{m g l \sin \theta_0} + m g l \cos \theta_0 \delta \theta = \cancel{\tau_0} + \delta \tau$$

$$m l^2 \ddot{\theta} + m g l \cos \theta_0 \delta \theta = \delta \tau$$

Perturbation about trim





$$\tau = mgl \sin \theta + du$$

$$ml^2 \ddot{\theta} + mgl \sin \theta = mgl \sin \theta + du$$

$$ml^2 \ddot{\theta} = du$$

Feedback Linearization



PUNT INVERSION

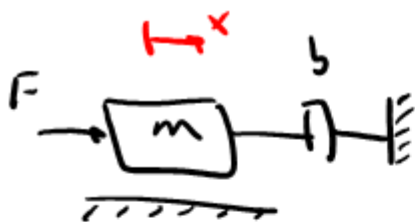




$\sin \theta \approx \theta$ if θ is small

Linearize & ignore





$$F - bv = m\dot{v}$$

$$m\dot{v} + bv = F + \phi$$

Σ, O, M

complex

Forced Natural/Homogenous

$$v = Ae^{st}$$

$$mAs e^{st} + bAs e^{st} = \phi$$

$$\dot{v} = As e^{st}$$

$$ms + b = \phi \rightarrow s = -\frac{b}{m}$$

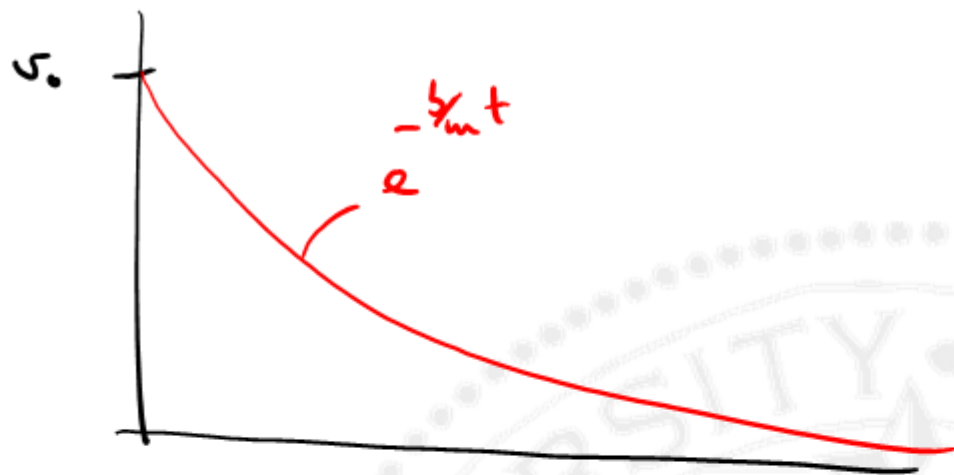
$$v = Ae^{-\frac{b}{m}t}$$

$$\rightarrow v(0) = Ae^{-\frac{b}{m}(0)} = A$$

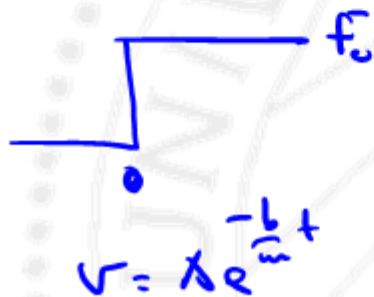
$$v(t) = v_0 e^{-\frac{b}{m}t}$$

← natural response





Forced Response



$$v_0 = \phi$$

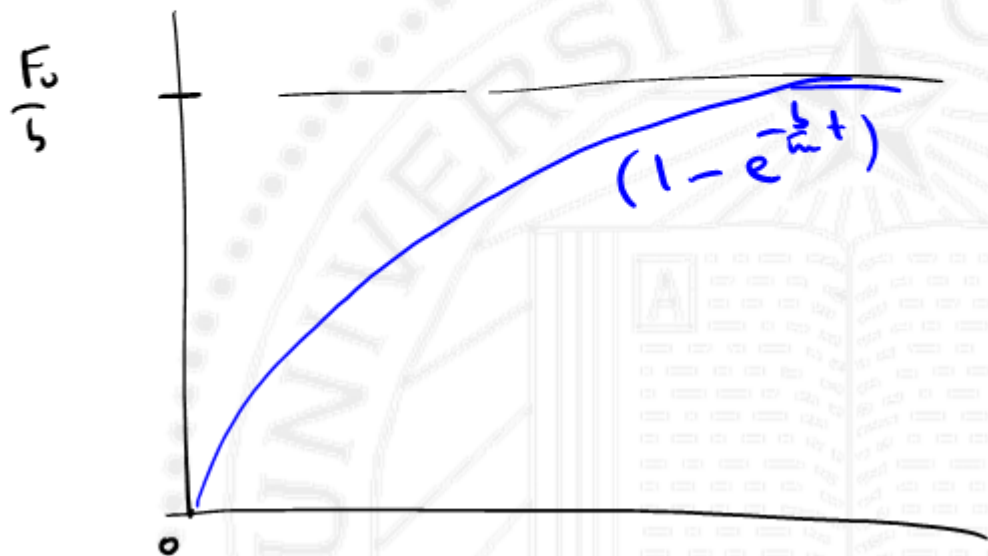
$$m/s + b v = F_0$$

$$v = \frac{F_0}{b}$$

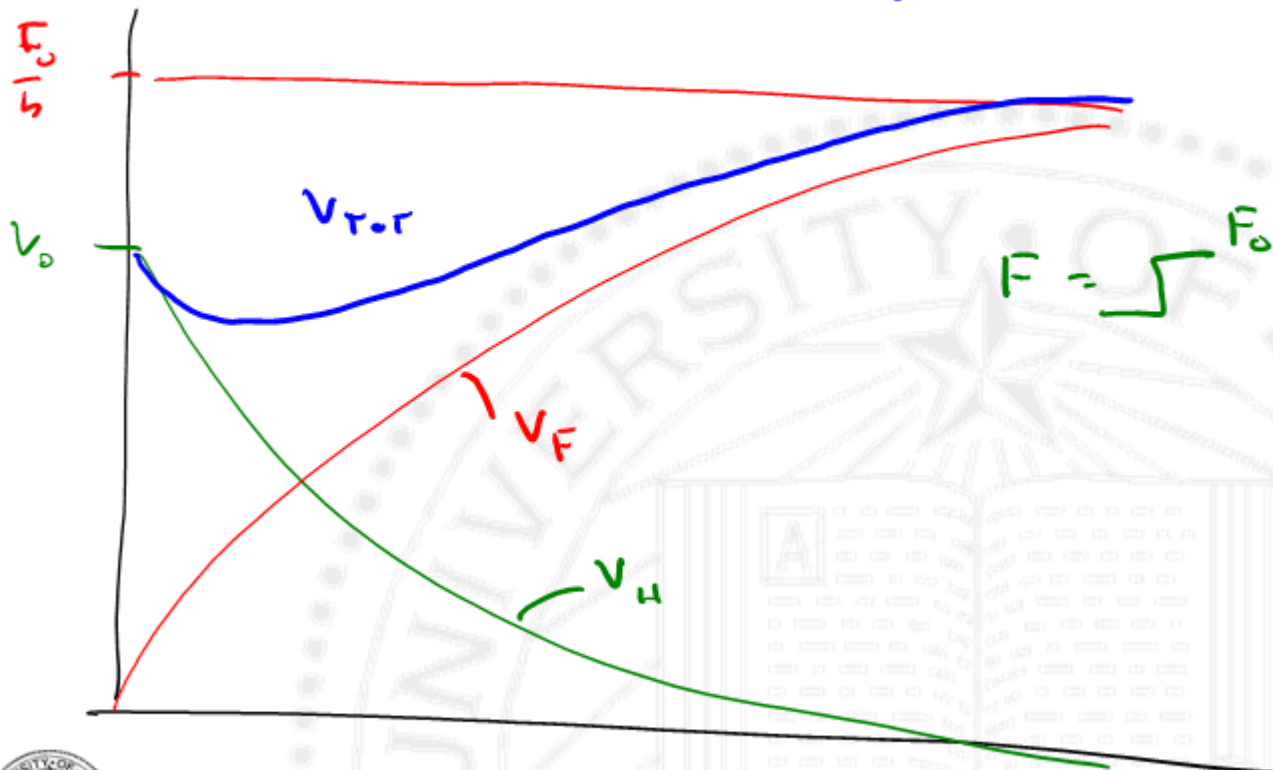


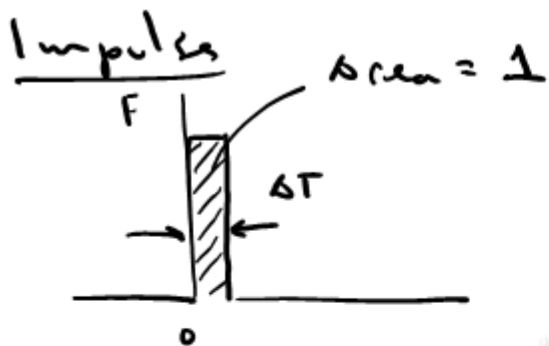
$$v = \frac{F_0}{b} + A e^{\frac{b}{m}t} \quad v(0) = 0. \quad 0 = \frac{F_0}{b} + A \quad \therefore A = -\frac{F_0}{b}$$

$$v_F(t) = \frac{F_0}{b} \left(1 - e^{-\frac{b}{m}t}\right)$$

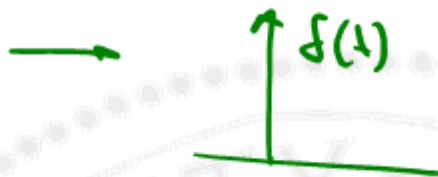


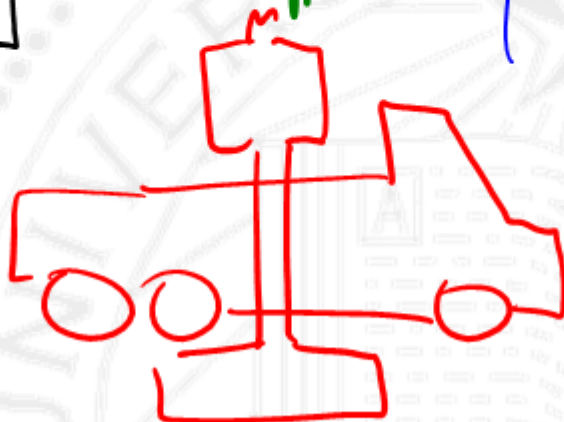
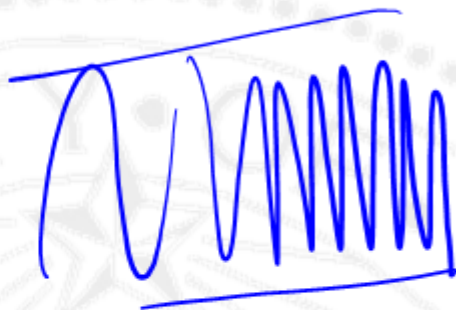
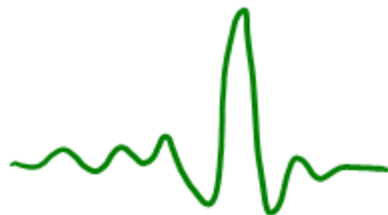
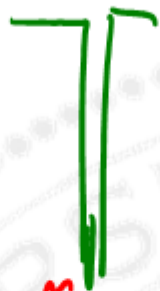
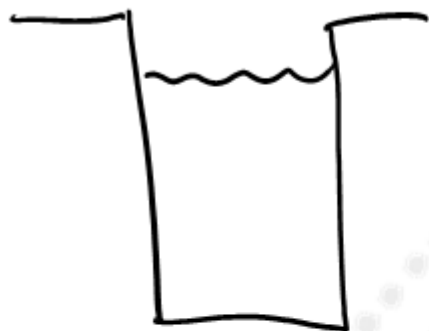
$$v_{TOT} = v_{NAT} + v_F = v_0 e^{-\frac{b}{m}t} + \frac{F_0}{b} (1 - e^{-\frac{b}{m}t})$$





$$\int f(t) dt = 1$$



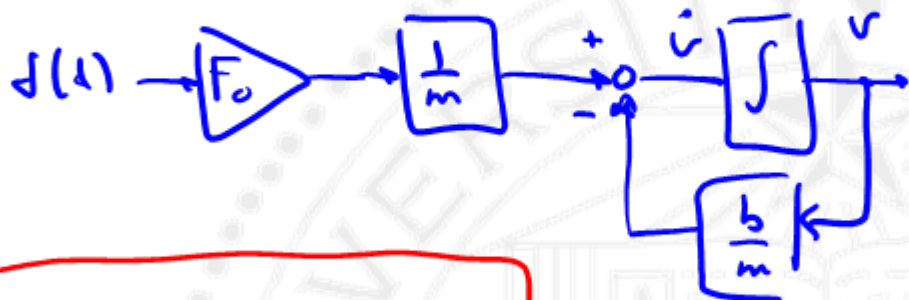


Impulse



$$\int \delta(t) dt = 1$$

$$m\dot{v} + bv = F_0 \delta(t)$$



$$0^+ : v = \frac{F_0}{m}$$

$$v_0 = \frac{F_0}{m}$$

$$v(t) = \frac{F_0}{m} e^{-\frac{b}{m}t}$$

